

Design and Fabrication of PET Bottles and Can Processing System

Hari Shanker

Department of Mechanical Engineering,
Ajay Kumar Garg Engineering College,
Ghaziabad, Uttar Pradesh, India, 201009
chaursiyahs@akgec.ac.in

Devendra Singh

Department of Mechanical Engineering,
Ajay Kumar Garg Engineering College,
Ghaziabad, Uttar Pradesh, India, 201009
singhdevendra@akgec.ac.in

Suman Gothwal

Department of Mechanical Engineering,
Ajay Kumar Garg Engineering College,
Ghaziabad, Uttar Pradesh, India, 201009
gothwalsuman@akgec.ac.in

Anubha Gupta

Department of Civil Engineering,
Ajay Kumar Garg Engineering College,
Ghaziabad, Uttar Pradesh, India, 201009
guptaanubha@akgec.ac.in

Abstract—Recycling is one of the sectors that is growing quickly these days. There is an enormous amount of rubbish pouring into PET bottles, and aluminium cans are two significant items being recycled more frequently. Crushers are utilised in this recycling process. To recycle these cans and PET bottles, enterprises rely on human labour, which is time-consuming and ultimately lowers production rates. We are developing an aggregate crusher system that uses a scotch yoke mechanism with multi-sided or dual-sided crushing capability in order to smash the cans and PET containers faster. PET bottles and aluminium cans of soda are crushed using a crusher machine for recycling reasons and for convenient storage in recycling bins once they have been shredded. The result entails successfully designing the various parts and components of the crusher unit while taking user ergonomics and forces into account.

Keywords: PET Bottles, Crushers, Al-alloy, Recycling, grey cast iron.

I. INTRODUCTION

Aluminium is a sustainable material that can be easily recycled, but it can take 80-100 years to decompose. The growing use of aluminium in the form of cans and bottles, if not recycled, can create significant environmental pollution [1]. Instead of electrolyzing aluminum, which must first be extracted from bauxite ore and then refined using the Bayer process, the procedure merely remelts the metal, which is significantly less costly and energy-intensive. Aluminium recycling accounts for only 5% of energy use, compared to fresh production, which simultaneously produces only 5% of greenhouse gas emissions. Aluminium-can recycling offers large benefits to the individual, community, government, economy, ecology and industry [2]. The US current rising percentage of aluminium can consumption is approximately 100 billion annually, as of 2025, and has a well-established curbside recycling infrastructure. Because of this, recycled scrap accounts for around 31% of all aluminium produced in the US [3]. Europe represents the second-largest regional market with a 28.1% revenue share as of 2025, driven by the European Union circular economy action plan. In the Asian Pacific fast-growing regional market, especially China and India, with rapidly urbanising middle-class populations, is shifting toward cans beverage

consumption and its share is projected to rise up to 22.8% as on 2025 [1]. Recycling soft metals, in this region, such as aluminium cans, is quite difficult due to the lack of quality recycling infrastructure and a large population [4]. Delivering goods to customers has been the mainstay of industrial activity in the modern era. Smashing cans is done by hand, which takes a lot of time and wears the operator down. Additionally, there are many different kinds of equipment, such as mechanical, hydraulic, and pneumatic ones, but they are expensive, big, and need operator supervision [5]. So, the manual crushing of aluminium cans and other packaging material of aluminium becomes tedious, time-consuming, has a low production rate and is rigorous. To improve this, a machine called a can crusher is used to crush it into a small volume, making it easy for storage and recycling. Different designs and modifications were done to improve the efficiency and effectiveness of the crusher as time passed. A solar panel-based can crusher is made to improve the energy efficiency and to reduce the environmental impact [6].

The mechanism used for crushing is either by applying an impact force, pressure or a combination of both. To reduce the effort required for crushing, the proper design of parts and components is necessary. Many researchers have tried to improve the design of some parts, and many have tried to reduce the weight, energy consumption and by using different materials [7-9]. Failure in the crusher's jaw is common and addressed in many studies to prevent the fatigue failure of the jaw and supporting bolts [10-14]. Parametric failure-based dynamic motion analysis 3D software, and process mapping analysis were used for individual parts and components [10, 15].

We are creating a can crusher machine with a multiple-sided crushing capability that uses a scotch mechanism to address this issue. The primary benefits include the capacity to crush multiple materials at a minimal cost and the ease with which even an inexperienced individual can handle it.

This report's only goal is to comprehend the basic concepts of operation and design. Simple mechanism features, including a fulcrum system, a single slider crank

mechanism, automation properties, etc., are used in this eco-friendly design. In order to significantly reduce the volume of the cans or bottles, considerable crushing power is required. The conceptualization is completed in a way that increases design, mechanism, and force understanding. The goal of this endeavor is to design and build an automatic can crusher machine while taking into account a number of crucial factors. In order to smash the cans as flat and geometrically as possible before they are shredded in the shredder, this project proposes to create a bottle or can crushing and shredding machine. It was crucial to complete this project in order to make sure that all that needed to be done was done, in addition to the manufacturing research. This project entails designing the various components of the crusher unit while taking user ergonomics and forces into account. The primary goal of this project is to come up with a novel idea for a can or bottle crusher that would be portable and make crushing the can or bottle simpler. Following completion, the design serves as a guide for the actual product.

II. MECHANISM USED

To reduce the effort required to crush the soft material cans and other packaging materials, a well-established mechanism called the slider crank mechanism is used. A reciprocating motion device, the Single Slider transforms a slider's linear motion into rotating motion or the other way around [16]. A connecting rod with a slot that engages a pin on the spinning element is directly connected to the piston or other reciprocating component. With a constant rotational speed, the piston's motion takes the form of a pure sine wave over time. Using this system, rotary motion can be transformed into reciprocating motion. To achieve the inversion, the cylinder must be fixed. Figure 1 shows that link 1 is fixed. A slider is represented by link 4, which reciprocates when link 2, which represents the crank, turns in this system [17]. To guide the Slider, the fixed link 1 is used.

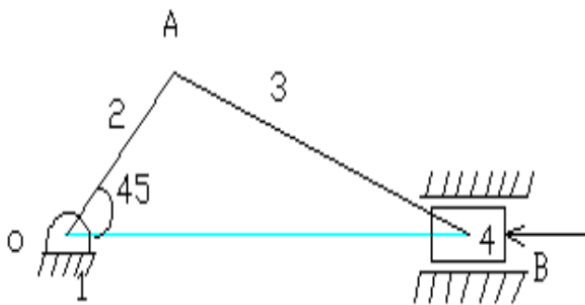


Fig. 1: Schematic of Single Slider Crank Mechanism [17].

III. WORKING

The schematic of the designed can crusher setup is shown in Figure 2. As the motor rotates, it has a smaller sprocket connected to its shaft; the smaller sprocket, through the chain, is connected to a secondary sprocket, which rotates it. There is another sprocket that is connected to the main sprocket through

a chain, which also rotates it. As the main sprocket rotates, it also rotates the main shaft, which in turn rotates the disk, and the whole mechanism starts working. When the disk rotates, the connecting rod also moves with it, which moves the piston left and right and crushes the cans during moving from its extreme points. The smashed bottles will enter the Shredder through the designated rectangular slots. The large volume of cans is converted into a small volume of crushed and shredded material that can be easily carried and recycled into finished products. The mass production can be ensured because it smashes the cans satisfactorily with a high production rate. The successfully constructed can crusher utilizing a single slider crank mechanism is given in Figure 2.

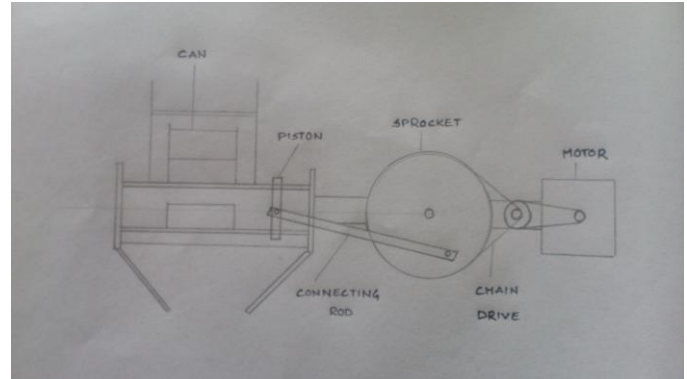


Fig. 2. Schematic view of the designed can crusher setup.

IV. DESIGN CONSIDERATION

The following parameters were considered during design and development:

- The greatest force needed to shatter the plastic bottles or cans.
- Parts and components taken in to considerations.
- The typical size of bottles and cans.
- Aluminum is the material for cans.

A. Design calculations

1. Determination of crushing force and Power

- The amount of force needed to shatter the plastic bottle.
- Power needed to shatter a soda or Pepsi can;
- Force needed to tear the can

So, we are considering the maximum of it.

Force is given by

$$\text{Force} = P_c * A$$

Where, P_c is crushing pressure = 15-41 ksi (15000-41000 psi) = 22.5 ksi (22500psi) or lbf/sq. inch = 155.13 MPa.
 A is area of crushing of can = $2 * 3.14 * R * t$
 R is the radius of the Can = $\text{Dia}/2 = 66.675/2 = 33.33$.
 $D = 2.5 - 2.8$ inch (assuming 66.675 mm).

t = The thickness of the wall of $C_{an} = 0.1$ mm

$$A = 2 * 3.14 * 33.33 * 0.1 = 20.9465 \text{ sq.mm.}$$

$$F = P_c * A = 155.13 * 20.9465 = 3.25 \text{ KN.}$$

- Power is given by

$$\text{Power} = F * V$$

Where V is the velocity of the piston.

F is the required crushing force.

V = piston movement/time.

Where, **Can height** = 5 inch = 0.127m.

Piston movement = 18cm = 0.18m.

Time = 1.275 sec

$$V = 0.18 / 1.275 = 0.141 \text{ m/s.}$$

$$\text{Power} = \text{force} * \text{velocity} = 3.25 * 0.141 = 0.5 \text{ KW} \\ = 0.683 \text{ hp.}$$

2. RPM of Sprocket

$$\text{Velocity} = 3.14 * D * N / 60$$

$$\text{Velocity} = 0.141 \text{ m/s.}$$

Where D is the Diameter of the Crank = 15 cm.

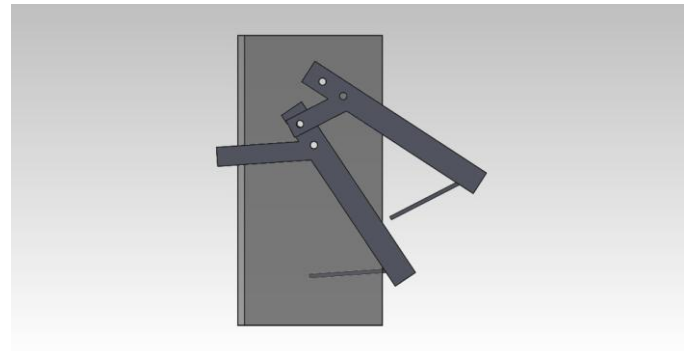
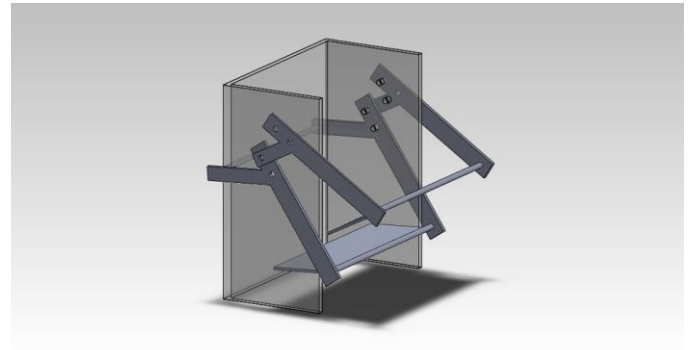
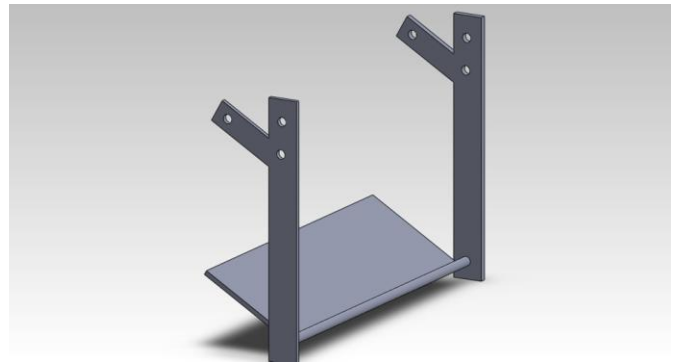
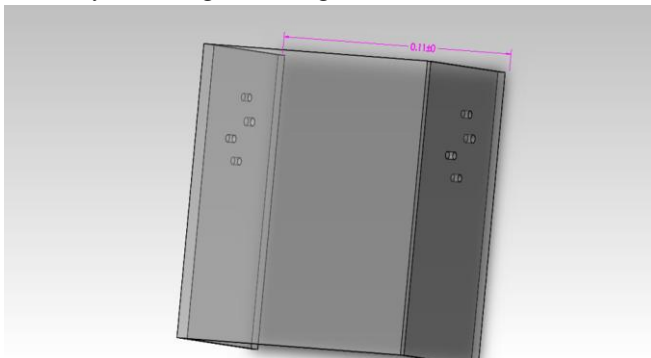
N is the rpm of the Sprocket.

$$0.141 = 3.14 * 0.15 * N / 60$$

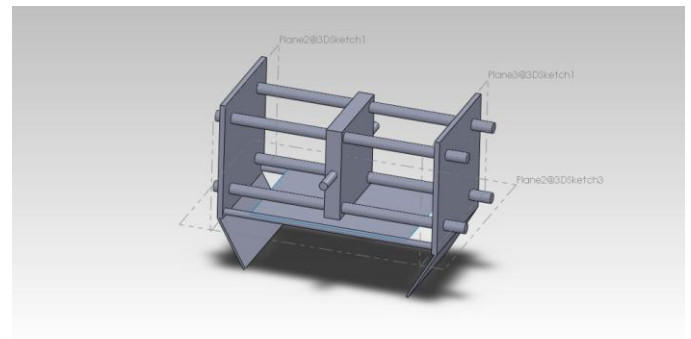
$$N = 18 \text{ rpm.}$$

2. Auto-feed Mechanism

The different parts and components of the auto feed system are given in Figure 3.



Crusher Mechanism



V. DESIGN OF COUPLINGS

A mechanical device that permanently connects two rotating shafts is called a coupling. Coupling is most frequently used to unite the shafts of two independently constructed or purchased units to create a new machine. To lift water from a well, for instance, a coupler connects the engine's output shaft to the hydraulic pump's input shaft. In industrial machinery, a coupling connects an input shaft of a gearbox to the output shaft of an electric motor. An electric motor's rotating shaft and a compressor's input shaft are connected through a coupling. The distinction between a clutch and a coupling is that a clutch allows the operator to join or separate two shafts, whereas a coupling is a persistent contact.

Rigid or flexible couplings are utilized when the axes are in the same line or collinear. A stiff coupling lacks the facilities necessary to tolerate a slight misalignment among the shafts, but a flexible coupling does.

The difference between rigid and flexible coupling is as follows:

A rigid coupling cannot tolerate misalignment between the axes of the shafts. It is only applicable when two shafts are precisely aligned. The flexible coupling, on the other hand, can withstand 5mm of axial misalignment and 0.5 degrees of angular misalignment between the shafts since it has flexible components like a bush or disk.

Shocks and vibrations are absorbed by the coupling's flexible components. In stiff coupling, such a provision does not exist. Only in situations where there are no shocks or vibrations may it be employed.

The following criteria should be met by a good coupling, whether it is rigid or flexible:

- It must be able to transfer torque from the driving shaft to the driven shaft.
- It must maintain the two shafts in the correct alignment.
- For repairs and modifications, the coupling should be simple to build and disassemble.

The material used for the flexible coupling is EN-GJS-800-2, which is grey cast iron with lamellar graphite with a yield strength of 1000-1100 MPa.

A. Design

Procedure for Flexible Coupling

Selection of material-
SHAFT-

Yield strength of material 1100 MPa

Factor of safety = 1

PINS-

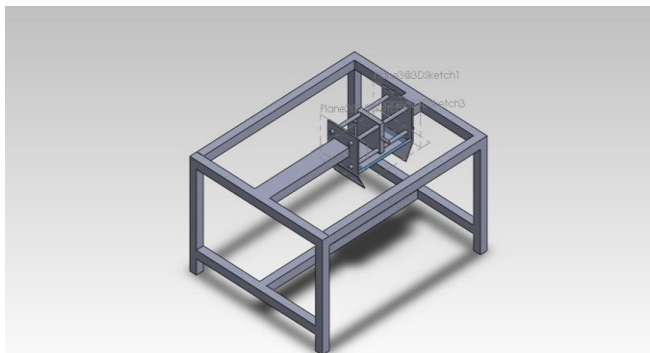
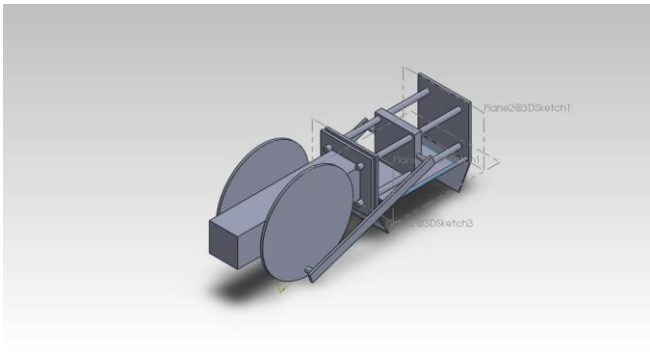
Yield strength of material = 400 MPa (plain carbon steel 30C8)

Factor of safety = 1

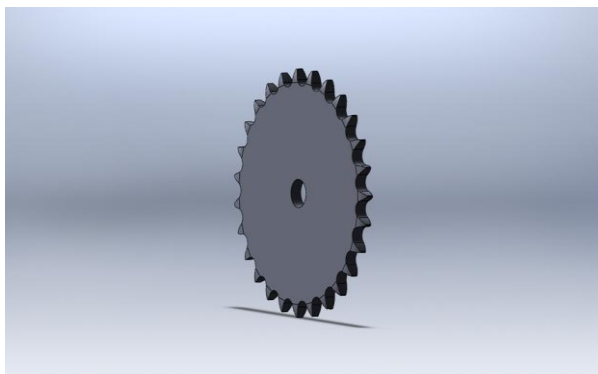
1. Permissible stresses:

• SHAFT-

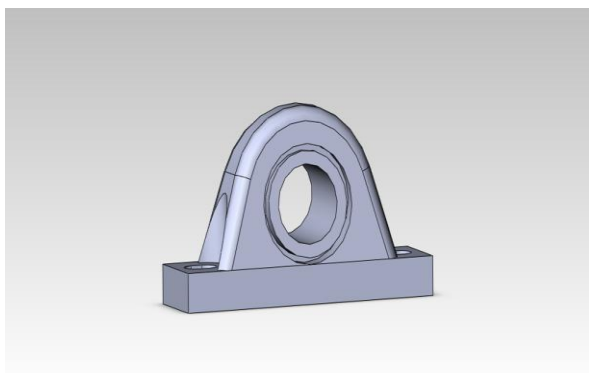
Torsional shear stress = $(0.5 \times \text{yield strength}) / \text{factor of safety}$



Casing



Sprocket



Bearing Block

Fig. 3. Different parts and components of a Can Crusher.

$$= (0.5 \times 1100) / 1 = 550 \text{ MPa.}$$

- **PINS-**

Torsional shear stress = yield strength/factor of safety
 $= 400 / 1 = 400$.

2. Diameter of Shafts:

The motor's starting torque is 125% of the rated torque.
 Therefore,

$$M = (60 \times 10^6 \times 0.745694 \times 1.25) / (2 \times 3.14 \times 18) = 494043.4692$$

$$\text{Torsional shear strength} = (16M / (3.14 \times d^3))$$

$$D = 15.78 \text{ mm or } d = 16 \text{ mm.}$$

3. Dimensions of Flanges:

- Outside diameter of hub = $2d = 32 \text{ mm}$.
- Length of hub = $1.5d = 24 \text{ mm}$.
- Pitch circle diameter of pins = $3d$ or $4d = 48 \text{ mm}$.
- Thickness of output flange = $0.5d = 8 \text{ mm}$.
- Thickness of protective rim = $0.25d = 4 \text{ mm}$.

Torsional shear strength M_r/J

$$M = 0.5 \times 3.14 \times d^4 \times t \times \text{torsional shear strength}$$

$$M = 843958.627$$

$$\text{Torsional shear strength} = 65.586 \text{ MPa} < 400 \text{ MPa}$$

So, the stresses in the flange are within the limit.

4. Diameter of Pins:

Number of pins selected, $N = 3$

$$\text{Diameter of pins} = (0.5 \times d) / \sqrt[3]{N} = 4.618 \text{ mm} = 8 \text{ mm}$$

(as per standardization)

$$\text{Shear stress in the pin} = (8 \times M) / (3.14 \times d^2 \times D \times N) = 328.044 \text{ MPa} < 400 \text{ MPa}$$

Therefore, based on shear resistance, its structure is secure.

B. Design Procedure for the Hub

1. Selection of material-

- **SHAFT-**

Yield strength of material = 690 MPa (High-strength alloy ASTM A514)

Factor of safety = 1.

- **PINS-**

Yield strength of material = 400 MPa (plain carbon steel 30C8)
 Factor of safety = 1.

Permissible stresses-

SHAFT-

$$\text{Torsional shear stress} = (0.5 \times \text{yield strength}) / \text{factor of safety} = (0.5 \times 690) / 1 = 345 \text{ MPa.}$$

PINS-

$$\text{Torsional shear stress} = \text{yield strength} / \text{factor of safety} = 400 / 1 = 400$$

Diameter Of Shafts

The starting torque of the motor is 125% of the rated torque. Therefore,

$$M = (60 \times 10^6 \times 0.745694 \times 1.25) / (2 \times 3.14 \times 18) =$$

$$494043.4692$$

$$\text{Torsional shear strength} = (16M / (3.14 \times d^3))$$

$$d = 19.393 \text{ mm or } d = 20 \text{ mm.}$$

3. Dimensions Of Flanges-

- Outside diameter of hub = $2d = 40 \text{ mm}$
 - Length of hub = $1.5d = 30 \text{ mm}$
 - Pitch circle diameter of pins = $3d$ or $4d = 80 \text{ mm}$
 - Thickness of output flange = $0.5d = 10 \text{ mm}$
 - Thickness of protective rim = $0.25d = 5 \text{ mm}$
- Torsional shear strength = M_r/J
 $M = 0.5 \times 3.14 \times d^4 \times t \times \text{torsional shear strength}$
 $M = 433539.7862$.
 Torsional shear strength = 36.8 MPa < 400 MPa
 So, the stresses in the flange are within the limit.

5. Diameter of Pins

Number of pins selected, $N = 4$

$$\text{Diameter of pins} = (0.5 \times d) / \sqrt[3]{N} = 5 \text{ mm} = 8 \text{ mm (as per standardization).}$$

$$\text{Shear stress in the pin} = (8 \times M) / (3.14 \times d^2 \times D \times N) = 138 \text{ MPa} < 400 \text{ MPa}$$

So, the shear strength of the design makes it safe.

C. Sprocket Design:

1. Selection of the Diameter:

Diameter of the sprocket attached to the Gear Box (Sprocket 1) = 100 mm

RPM available at the output of the Motor = 1440

Gear Ratio of the Gear Box = 40:1

Therefore,

RPM available at the output of the Gear Box, i.e., at the sprocket 1 = $1440 / 40 = 36$.

RPM required at the crank = 18.

Therefore

$$\text{Diameter of the Sprocket attached to the shaft will be} = (36 / 18) \times 100 = 200 \text{ mm.}$$

Material of the Sprocket – Tempered and Case-Hardened Steel

Strength of the Sprocket material- 900 MPa

Assuming, FOS = 1.3

Available strength of the Sprocket material = $900 / 1.3 = 700 \text{ MPa}$.

2. Selection of Pitch and Pitch Circle Diameter:

Since the RPM at the Sprocket 1 is 36 (low-speed applications)
 Therefore,

The selected pitch is **13 mm**

PCD of sprocket 1 = 80 mm

PCD of sprocket 2 = 170 mm.

D. Chain Design:

The strength of the chain material should be higher than that of the sprocket material; otherwise, there would be a lot of wear and tear on the teeth of the sprocket.

Therefore

Strength of the Chain material = 1500 MPa

Material of the Chain – Alloy Steel.

E. Bearing Design:

We have selected Ball Bearing due to the following advantages-

- Due to the point contact, there would be low friction.
- It can sustain axial and radial load simultaneously.
- It has a high load-carrying capacity.

RPM of the shaft = 18

Radial load on the bearing = Weight of 2 sprockets

Weight of shaft + Additional weight
= 80+80+40+40 = 240 N

Axial load on the bearing = Zero

Therefore

Equivalent load on the bearing, $P = 240 \text{ N}$.

Now,

Diameter of the shaft = 20mm (as the ID of the sprocket is 20mm)

Life required = 60000 hours.

Therefore,

$L_{10} = (60 \times N \times L) / 1000000$

$= (60 \times 18 \times 60000) / 1000000 = 62.4 \text{ million}$

revolutions.

Therefore

Dynamic load carrying capacity, $C = P (L_{10})^{0.33} = 240 \times (62.4)^{0.33} = 950 \text{ N}$.

Available Bearing ---- 61804

Dynamic load carrying capacity = 2700 N.

F. Design of Gear Box

Worm reduction gear unit under driven type is required to drive a sprocket and chain, medium loaded, operating 24 hrs per day at 36 rpm, transmitting 0.746 KW. The gear unit is directly driven by a coupling by a 1440 rpm electric motor. The ambient temperature is 30 degrees on the machine.

STEP 1:

Ratio required = Input speed/Output speed = 1440/36 = 40:1.

STEP 2:

From Table 1

Driven machine- sprocket chain (medium loaded)

Type of load- moderate shock

From Table 2

Mechanical service factor (F_m)= 1.50 for 24 hr/day continuous operation.

STEP 3:

Equivalent output power (mechanical) = $0.746 \times 1.5 = 1.119 \text{ KW}$.

Equivalent output torque (mechanical) = $(9550 \times 1.119) / 36 = 296.845 \text{ Nm}$

From catalogue

Refer rating at input speed 1440 rpm, ratio 40:1

Gear unit size 12, ratio 40:1, having output torque (mechanical) = 296.845Nm

Input power (mechanical) = 62 KW.

STEP 4:

From table 3, thermal service factor (F_t) = 1.16

For an ambient temperature of 30 degrees

Equivalent output power (thermal) = $0.746 \times 1.16 = 0.86536 \text{ KW}$
= $(9550 \times 1.119) / 36 = 296.845 \text{ Nm}$.

STEP 5:

From the catalogue, rating at input 1440 ratio- 40:1 for 12-inch size

The Output torque (thermal) = 296.845Nm,

Which is less than the calculated equivalent

The Output torque (thermal) = 280 Nm

Required input power = (calculated equivalent output torque(mechanical) * Rated power(mechanical) / (rated output torque * F_m))

VI CONCLUSION AND FUTURE SCOPE

The working and performance of any robust system depend on the material used, its design parameters, and manufacturing considerations as per the applications. After proper design of each part and component, the research work leads us to the conclusion that it can be employed in mass production because it smashes the cans satisfactorily in a short amount of time, which leads to high recycling ability to crush the cans. After a robust design, a can crusher was successfully constructed utilising a single slider crank mechanism. The can crusher is well designed with robust parts and components and has been tested. The theoretical design seems well established, but it can be improved by applying some design software, so that the fabrication process and design parameters can be improved.

REFERENCES

- [1]. S. A. Buza, K. A. Buza and K. Pillana, "Can crusher design in response to environmental concerns", Journal of Trends in the Development of Machinery and Associated Technology, Vol. 18, No. 1, pp. 179-182, 2014.
- [2]. S. Bhat, D. Patel, V. Chandola, "Can Crushers Market Research Report 2034" Segments - by Product Type Manual, Automatic, Semi-Automatic Can Crushers, by Material (Steel, Plastic, Aluminium, Others), by Application (Residential, Commercial, Industrial), by Distribution Channel, Report ID: CG-40758, 5.0 Rating, 17 May 2026, 277 Pages.
- [3]. R. Krushna, S. More, and S. J. Rajpal, published a review paper on "Study of Jaw Plates of Jaw Crusher". International Journal of Modern Engineering Research (IJMER), Vol. 3, Issue.1, Jan-Feb. 2013 pp. 518- 522 ISSN: 2249-6645.
- [4]. S. Husain and M. S. Sheikh, presented a paper on "Can crusher machine using scotch yoke mechanism". IOSR Journal of Mechanical and Civil Engineering (IOSR-JMCE) e-ISSN: 2278-1684, p-ISSN: 2320-334X PP 60-63.
- [5]. C. Mohd, A. Akasyah, B. C. Anuar, Faculty of Mechanical Engineering, University Malaysia Pahang, in the year November 2008, in his project report entitled "Development of the Can Crusher Machine".
- [6]. A. Elfakhany, "A new Patent of Beverage Cans Crusher Machine", Current Alternative Energy, Vol. 2, pp. 123-131, 2018.
- [7]. V. N. Kshirsagar, S.K. Choudhary, A.P. Ninawe, "Design Consideration in an Automatic Can/Plastic Bottle Crusher Machine", International Journal of Engineering Research and General Science Volume 2, Issue 4, June-July, 2014.
- [8]. Durgesh, R. Verma, and P. R. Hatwar, "Design of A Horizontal Shaft Impact Crusher", International Journal of Application or Innovation in Engineering & Management (IIAEM), Volume 3, Issue 1, January 2014.

- [9]. Ramakrishna, S. More, S. J. Rajpal, "A Review on Study of Jaw Plates of Jaw Crusher", International Journal of Modern Engineering Research (IJMER), Vol. 3, Issue.1, Jan-Feb. 2013 pp-518-522.
- [10]. E. Rusiński, P. Moczko, D. Pietrusiak, G. Przybyłek, "Experimental and Numerical Studies of Jaw Crusher Supporting Structure Fatigue Failure", Strojnicki vestnik - Journal of Mechanical Engineering 59(2013)9, 556-563.
- [11]. A. K. Shrivastava, A. K. Sharma, "Dynamic Analysis of Double Toggle Jaw Crusher Using ProMechanica", International Journal of Engineering Research and Applications, Vol. 2, Issue 3, May-Jun 2012, pp.1132-1135.
- [12]. A. Refahi, J. A. Mohandesi, and B. Rezai, "Comparison between bond crushing energy and fracture energy of rocks in a jaw crusher using numerical simulation", The Journal of The Southern African Institute of Mining and Metallurgy volume 109 refereed paper December 2009.
- [13]. E. Elisante, "Simplification of Jaw crusher for Artisanal Aggregates Miners", Journal of Engineering and Technology Research Vol. 1 (6), pp. 102-108, September, 2009.
- [14]. S. Choudaha, S. K. Tiwari, S. Pande, "Improving Productivity of Jaw Crusher through OTIF Delivery by Reducing Down Time", International Journal of Emerging Technology and Advanced Engineering Website: www.ijetae.com (ISSN 2250-2459, Volume 2, Issue 10, October 2012).
- [15]. C. Jinxi, Q. Zhiyu, R. Xingfu, and Y. Shichun, present a paper on "Experimental Research on Crushing Force and its Distribution Feature in Jaw Crusher" at the 2007 Second IEEE Conference on Industrial Electronics and Applications. 1-4244-0737- 0/07/\$20.00© 2007 IEEE.
- [16]. T. Gao, J. Cao, D. Zhu, and J. Zhi, present a paper on "Study on Kinematics Analysis and Mechanism Realisation of a Novel Robot Walking on Water Surface". Proceedings of the 2007 IEEE International Conference on Integration Technology, March 20 - 24, 2007, Shenzhen, China. 1-4244-1092-4/07/\$25.00 © 2007IEEE.
- [17]. Design data for machine elements by B. D. Shiwalkar, 2013 edition and a Textbook of Machine Design by R.S. Khurmi and J. K. Gupta, 14th revised edition, S. Chand publication.